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Simulation of protection functions in LV shipboard electrical power systems

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Abstract. The basic function of a shipboard electric power systems is to supply all consumers, both essential and non-essential, with electrical energy, as economically as possible and with an acceptable degree of quality. A shipboard electrical power system comprises three principal subsystems: generation (naval power plant-island mode plant), distribution and protection and automation. During operation all these subsystems may be affected by faults. In this aim all electrical installations on shipboards are to be protected against over-currents due to short-circuits or accidental overloads. The new ABB air circuit-breakers Emax 2 and Tmax T series can be used both as main circuit-breaker in low voltage generation and distribution systems. In addition to protection, the new air ABB circuit-breakers offer possibility of communication which are particularly suitable for automation, control, measurements, grid analysis, and energy savings. ABB Relays are high-performance electronic units for these circuit breakers. Their basic function is to monitor and protect the electric systems against fault current. The units also includes: measuring, data storage, communication, self-test, load control and zone selectivity functions for these circuit-breakers. This paper presents the analysis of protections and simulates how to trigger protections within shipboard power systems.

1. Introduction

A protection relay is a special type of relay which monitors the following electrical parameters such as: [1]

- intensity of current $I[A]$
- voltage $U[V]$
- frequency $f[Hz]$
- active power $P[W]$

from a generating source (alternators) or loads (electric motors and power transformers) with the purpose triggering one or more circuit breakers to open an one circuit or more circuits (feeders) in the case of a fault condition (overloads and short-circuits). For example in the low voltage shipboard power systems the protective function are implemented inside the circuit breaker itself.

The aim of protective relays are:

- to increase the shipboard safety of electric power systems
- to avoid the black-outs
- to prevent alternators, electric motors, power transformers damage in advance
- to be able detect already occurred faults (overloads and short-circuits) to limit further damage of electrical equipment

2. MNS 3.0 low voltage main switchboard for shipboard applications

Each section of MNS 3.0 LV main switchboard is divided into more compartments (cubicle) thus separating different functional zones (figure 1 and figure 2) [3]:

- Incoming circuit breaker technical solution
 - Electrical equipment compartment (circuit breaker compartment)
 - Bus-bar systems compartment
- Outgoing solution
 - Electrical equipment compartment (motor starter modules – motor control centre MCC)
 - Cable compartment (power cables and control cables, terminals and connection units)
 - Bus-bar system compartments

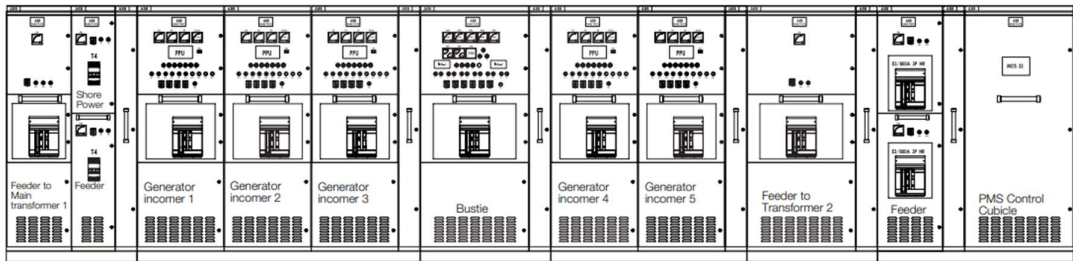


Figure 1. A general arrangement drawing and single line diagram of MNS 3.0

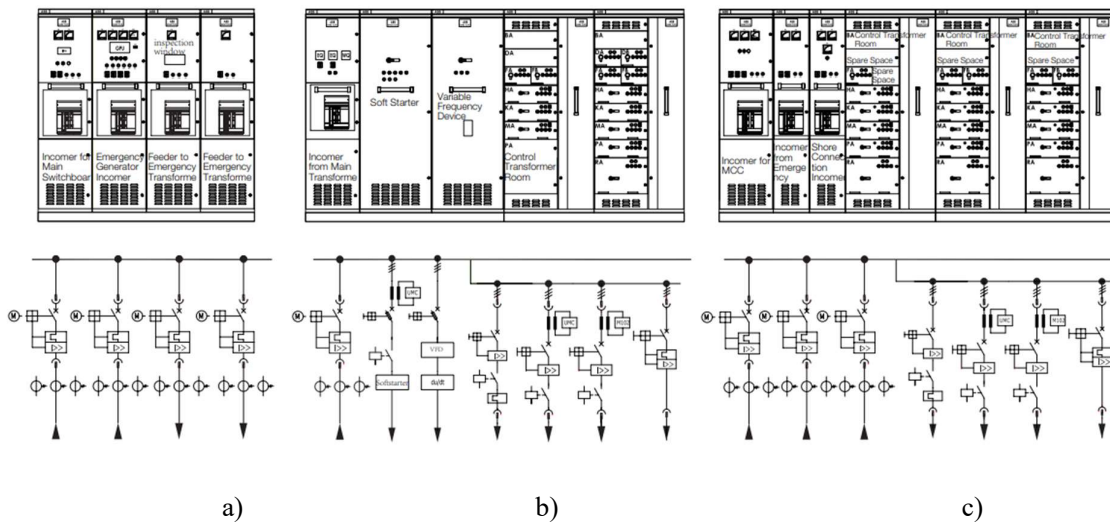


Figure 2. MNS 3.0

- a) Emergency Switchboard
- b) MCC (motor control centre) cubicle
- c) Emergency MCC (motor control centre) cubicle

In order to satisfy all requirements there are three main switch incoming options (figure 3):

- Load break switches
- Molded case circuit breakers (MCCBs)
- Air circuit breakers (ACBs).

In addition to the above ABB circuit breakers offer a series of integrated programmable releases (PRs), where combinations of protection functions may be selected with [3]:

- Overload protection (LTD – long time delay)– L
- Selective short circuit protection (STD – short time delay)– S
- Instantaneous short circuit protection (INST – instantaneous)– I
- Earth (ground) fault protection – G (in case of alternators)



Figure 3. 3D view of the MNS breaker compartment and Emax breaker with PR123/P trip unit

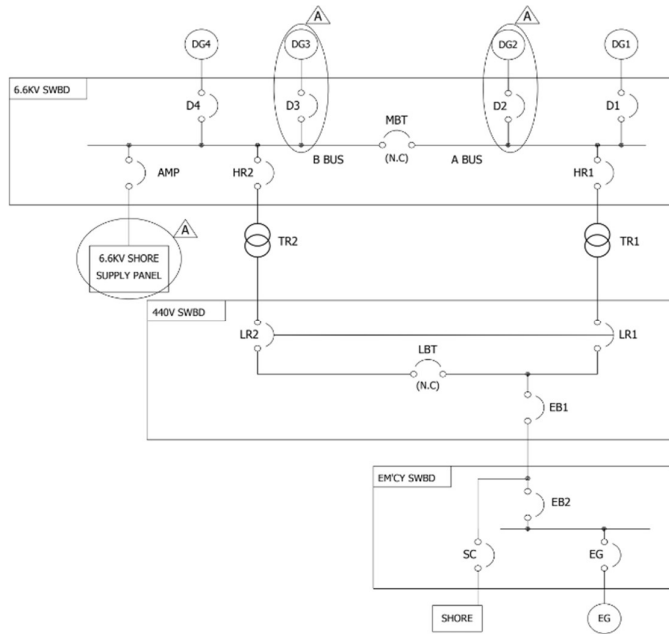


Figure 4. Synchronizing and distribution cubicle of MNS 3.0

3. Single line diagram of shipboard power systems and time-current characteristics

In order to simulate the protections as input data, the following are taken into account [2], [7], [8]:

- single line diagram of electric power system (figure 5)
- ACB (air circuit breaker) trip setting list and trip diagram (LSI) (figure 6)
- Single line diagram of protection systems and measuring and control equipment (figure 7)



- 1) LR1 AND LR2 ARE MUTUALLY INTERLOCKED. WHEN MBT IS CLOSED, LR1 AND LR2 CAN BE CLOSED AT A TIME FOR THE CHANGE-OVER WITHOUT BLACK OUT. WHEN LBT IS OPENED, THE INTERLOCKING BETWEEN LR1 AND LR2 WILL BE RELEASED.
- 2) MBT AND LBT ARE CLOSED NORMALLY.
- 3) MBT CAN BE CLOSED WITH MANUAL SYNCHRONIZATION WHEN BOTH SIDES OF MBT ARE ALIVE.
- 4) LR1(LR2) CAN BE CLOSED ONLY WHEN HR1(HR2) IS CLOSED.
- 5) LR1(LR2) WILL BE OPENED AUTOMATICALLY WHEN HR1(HR2) IS OPENED.
- 6) HR1(HR2) WILL BE OPENED AUTOMATICALLY WHEN LR1(LR2) IS OPENED.
- 7) THE 6.6KV SWBD IS FITTED WITH A SHORT CIRCUIT FAULT DETECT CIRCUIT. IN THE EVENT OF A BUS SHORT CIRCUIT FAULT, THE FOLLOWING BREAKERS ARE ELECTRICALLY PREVENTED FROM BEING CLOSED.
A) SHORT CIRCUIT FAULT ON 6.6KV SWBD A BUS SIDE → D1, D2 AND MBT
B) SHORT CIRCUIT FAULT ON 6.6KV SWBD B BUS SIDE → D3, D4 AND MBT
- 8) SC CANNOT BE CLOSED WHEN DG FEED THE 440V SWBD.
- 9) SHORE & EG CANNOT SUPPLY POWER TO 6.6KV SWBD.
- 10) EB1 IN 440V SWBD IS CLOSE NORMALLY AND HAVE TO BE CLOSED MANUALLY.

Figure 5. Single line diagram of Electric Power System of container ship

CIRCUIT		HM1502A~V HM2302A~V	BUS TIE	LM1215A~D		
AIR CIRCUIT BREAKER	TYPE	UAN-63D(MRD)	UAN-63D(MRD)	UAN-08A(MRD)		
	NUMBER OF POLE	3P	3P	3P		
	VOLTAGE	AC 450V	AC 450V	AC 450V		
	FREQUENCY	60Hz	60Hz	60Hz		
	AMPEREFRA	6300AF	6300AF	800AF		
	BASE CURRENT	I _{ct} In	6300A 5004A	6300A 700A		
	OVERCURRENT TRIP	TYPE	UPR-SA	UPR-SA	UPR-SA	
		PICK UP CURRENT I _r = I _n x RANGE	RANGE	0.8-1.25-NON	0.8-1.25-NON	0.8-1.25-NON
		SET AMP	1.0 5004A	NON -	1.0 700A	
		OPERATING TIME(I _r x120%)	40SEC AT I _r x120%	40SEC AT I _r x120%	40SEC AT I _r x120%	
SHORT TIME DELAY TRIP (STD)	PICK UP CURRENT I _{st} = I _o x RANGE	RANGE	2.0-5.0-NON	2.0-5.0-NON	2.0-5.0-NON	
	SET AMP	3.0 15012A	2.0 12600A	4 2800A		
INST TRIP	OPERATING TIME	400mSEC	300mSEC	200mSEC		
	PICK UP CURRENT I _i = I _o x RANGE	RANGE	4-16-NON	4-16-NON	2-15-NON	
TRIPPING DEVICE	UVT OR SHT	UVT(0.5 SEC)				
	TYPE	UAN5-V2				
	OPERATING TIME					
	OPERATING VOLTAGE					

<< NOTE >>
 1. ACB TYPE DESIGNATION
 UAN-63 - M R D
 (1) (2) (3) (4)
 (1) ACB TYPE
 (2) CLOSING MECHANISM
 E- ELECTROMAGNETIC SOLENOID OPERATION
 M- STORED ENERGY (MOTOR & MANUAL CHARGE)
 H- STORED ENERGY (MANUAL CHARGE)
 (3) OVERCURRENT TRIP DEVICE
 R (APR)-SOLID STATE TYPE LTD & STD TRIP
 L (APL)- THERMAL MAGNETIC TYPE STD TRIP
 N - NONE
 (4) MOUNTING
 F- FIXED TYPE
 D- WITHDRAWABLE TYPE
 2. INST TRIP DEVICE
 AIT - ELECTROMAGNETIC TYPE INST TRIP
 3. DEFINITION OF EACH CURRENT AND OPERATING TIME

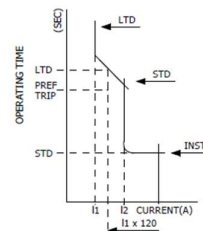


Figure 6. ACB trip settings list and trip diagram

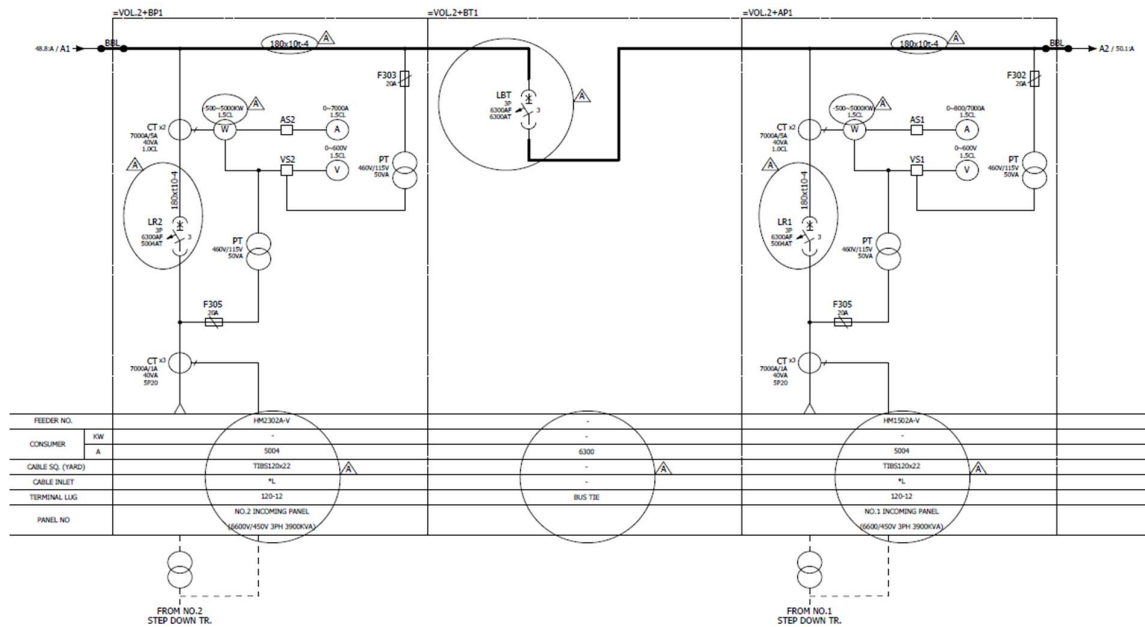


Figure 7. Single line diagram of protection systems, measuring and control equipment

4. Protection simulation results with the ABB PR123/P trip unit

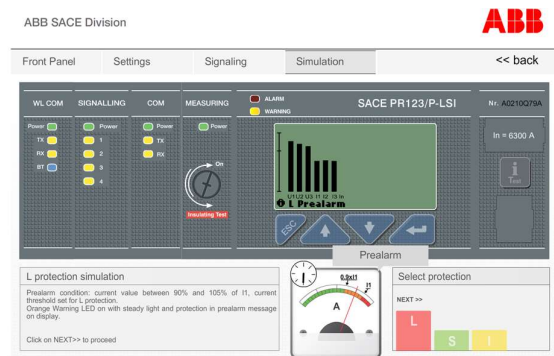
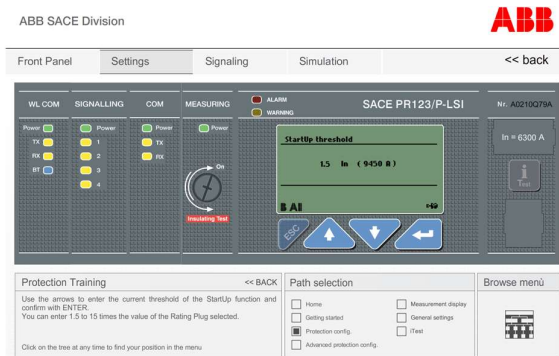
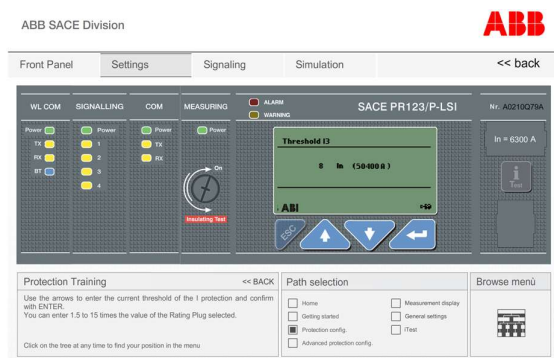
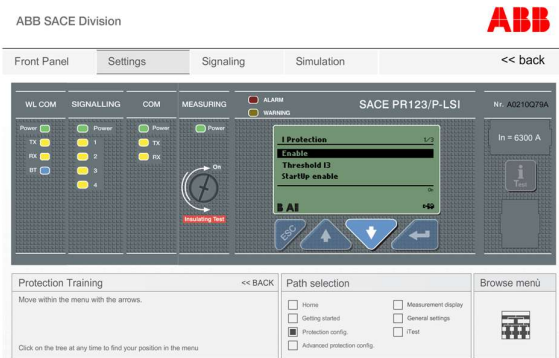
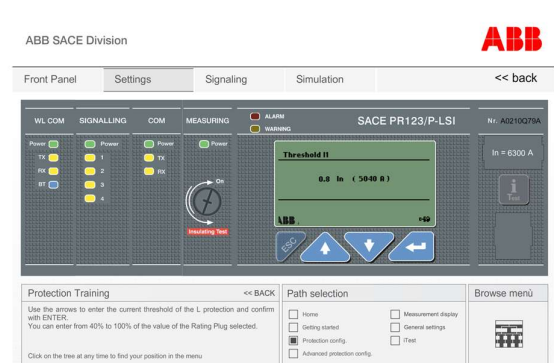
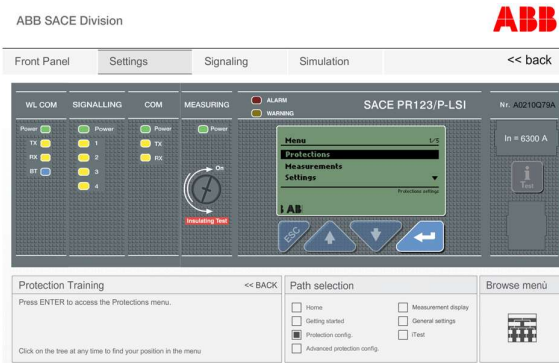
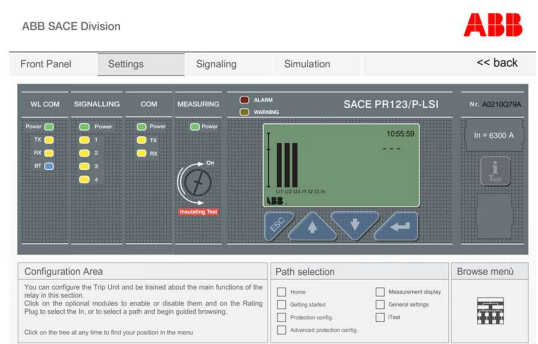
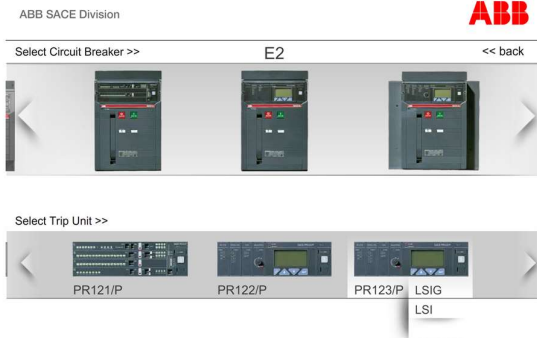
ABB PR123/P is a high-performance trip unit, capable of offering a complete set of functions for protection, measurement, signalling, data storage, command and control of the low voltage Emax series of ABB air circuit-breaker.

The protection functions of PR123/P trip unit are [4], [5], [6], [9], [11]:

- overload (L) (In accordance also with IEC 60255-3 Standard)
- selective short-circuit (S)
- instantaneous short-circuit (I)
- earth fault with adjustable delay (G) (The current values is disabled and are indicated in the installation manual)
- directional short-circuit with adjustable delay (D)
- phase unbalance (U)
- protection against over-temperature (OT)
- load control (K)
- under-voltage (UV)
- overvoltage (OV)
- residual voltage (RV)
- reverse power (RP) (only in the case of generators)
- under-frequency (UF)
- over-frequency (OF)
- phase sequence (alarm only).

The data presented in Figure 6 are used to simulate the tripping of protection for HM1502A ~ V HM2302A ~ V circuits.

Figure 7 shows the protection simulation results using the PR123/P trip unit. ABB trip simulator was used to achieve this.



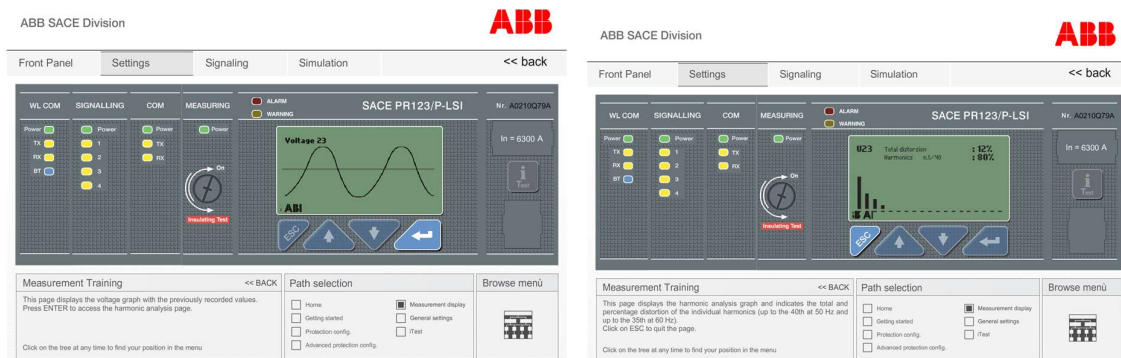


Figure 8. Protection simulation results with the PR123P trip unit that equips the ABB EmaxX1 circuit breakers

5. Conclusions

The protection relay of an electrical networks as complex as electrical ship power plants must be designed as a whole. The process of designing protection systems is laborious and difficult because it requires the calculation of short-circuit currents in order to choose the switching equipment.

Figure 8 shows the steps of the simulation algorithm for the main protection functions: overload (L), selective short-circuit (S) and instantaneous short-circuit (I). For this, the ABB simulation program was used with the electronic circuit breaker trip unit SACE PR123/P which includes three main parts: settings, signalling and simulation of protection functions.

Also another important feature of the trigger unit is the ampere-frame. In the simulation presented in figure 8 the value of the nominal current of two identical circuits is 5004A. Particular importance must be paid to the correct choice of circuit breaker tripping unit.

The tripping threshold of the protection is calculated according to the rated current for both overload protection and short circuit protection. At the same time, a correct evaluation of the short-circuit currents as a result of the thermal and electro-dynamic effects resulting from their occurrence is necessary. As can be seen from Figure 7, the two circuits have the same rated current because the two 6.6 / 0.45kV distribution transformers have the same nominal rated power of 3900kVA. The rated current corresponding to the choice of the two circuit breakers LR1 and LR2 is the rated current of the secondary winding of the two identical transformers.

The PR123/P trigger unit also includes the measurement part of the main electrical parameters (currents, voltages, powers, power factor, THD, energies). During the measurement simulation, only two parameters were analysed, namely voltage wave and total harmonic distortion.

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