GOOD PRACTICE EXAMPLE: DESIGNING 100KN DELTA EYE PLATE

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Abstract: This article is presenting the steps carried for the design process of a 100KN delta eye plate, which is a simple but important element used in different setups for offshore installation, by using CAD/CAE methods applied on ANSYS 12.1 Workbench.

Keywords: CAD/CAE, shear stress, distortion.

A general single towing arrangements consists in:

- A short pennant the connection from tug to delta eye plate
- One delta eve plate
- Two bridles (from delta eye plate to the vessel sides)
- Two chafing chains from the bridles to the tow connections

Short pennant

Delta eye plate

Wire rope bridle (steel wire or chain)

Chafing chain

Recovery wire

"A" frame or shaft strut

Tow connection

Recovery winch

Figure 1 A typical pulling arrangements (Referinta)

One of the key points of the tugging arrangements, is the delta eye plate.

In this plate it is concentrated the tug force and it is distributed on the vessel sides.

In this paperwork we will present the designing steps for a 100KN delta eye plate, using CAD/CAE methods on ANSYS 12.1 Software.

First of all, it is necessary to create the geometric model of the plate.

In a 221mm equilateral triangle we are drawing another 100mm equilateral triangle. The big

triangle represents the delta eye plate and the small triangle corners represent the center of 3x40mm holes.

The delta eye plate have 40mm thickness.

The 221mm triangle corners are blended at a 35mm radius.

The delta eye plate looks like in figure:

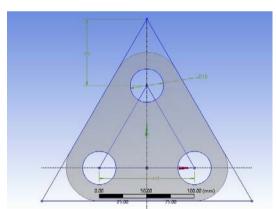
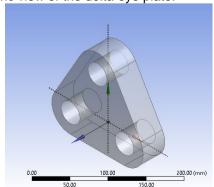


Figure 2 Side view of the 100 KN delta eye plate

Isometric view of the delta eye plate:



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Figure 3 Isometric view of the 100 KN delta eye plate

In practice, the delta eye plate must be realized at it was described, using AH36 structural steel plate.

For the structural analysis during towing, there were added 40mm pins in the holes.

The entire ensemble looks like below:

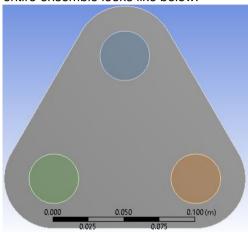


Figure 4 Side view of the towing arrangements

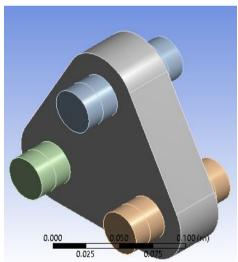


Figure 5 Isometric view of the towing arrangements

The next step in designing the plate is meshing. Mesh characteristics are presented below:

Defaults	
Physics Preference	Mechanical
Relevance	100
Sizing	
Use Advanced Size Fun	Off
Relevance Center	Coarse
Element Size	5.e-003 m
nitial Size Seed	Active Assembly
Smoothing	Medium
Transition	Fast
Span Angle Center	Coarse
Minimum Edge Length	4.e-002 m

Figure 6 Details of the mesh

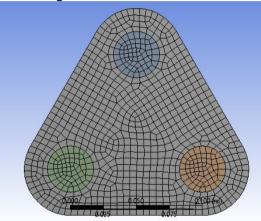


Figure 7 Side view of the mesh structure

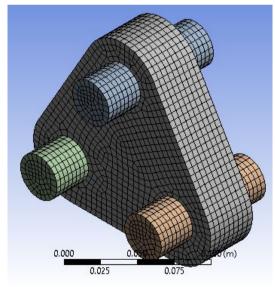


Figure 8 Isometric view of the mesh structure

The mesh consists in 52192 nodes and 11160 elements.

After meshing, the next step consists in setting up the boundary conditions which are:

- Earth gravity is active,
- The 100KN force acts on one of the bolts, on the OY direction
- The other are two bolts are fixed.

Boundary conditions are presented in following picture:

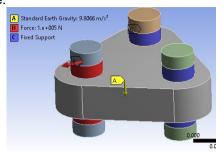


Figure 9 Boundary conditions

Last step is the structural check. Results of the structural check are presented bellow:

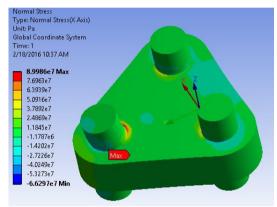


Figure 10 Normal Stres on X axis

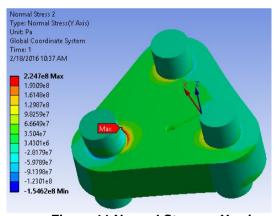


Figure 11 Normal Stres on Y axis

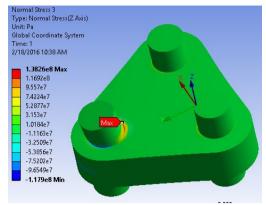


Figure 12 Normal Stres on Z axis

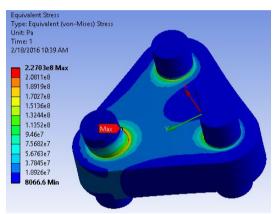


Figure 13 Equivalent Stres

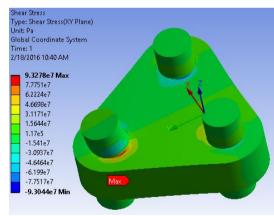


Figure 14 Shear Stress (XY Plane)

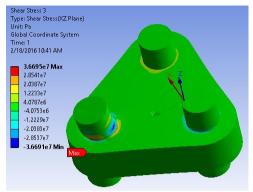


Figure 15 Shear Stress (XZ Plane)

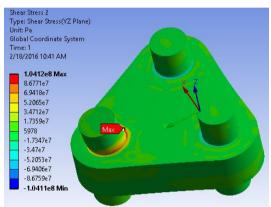


Figure 16 Shear Stress (YZ Plane)

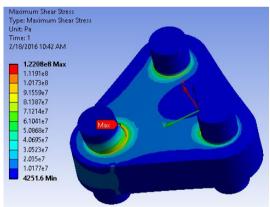


Figure 17 Shear Stress

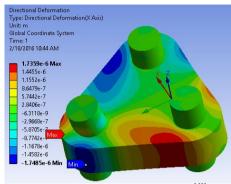


Figure 18Deformations on X Axis

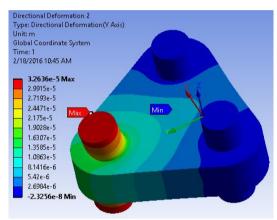


Figure 19 Deformations on Y Axis

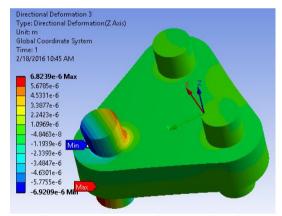


Figure 20 Deformations on Z Axis

The AH36 structural steel have the elastic limit at 355N/mm² (3.55E8 Pa). The maximum equivalent stress at this plate, having the design force on one bolt, is at about 63.9% of this limit, which is accepted by all the classification societies.

BIBLIOGRAPHY

[1] Ansys Workbench User Manual

[2] Huei – Huang Lee, Finite Element Simulations with Ansys Workbench 12, Schroff Development Corporation, ISBN 978-1-58503-604-2, 2010,

[3] Moaveni Saeed, Finite Element Analysis: Theory and applications with Ansys, 3rd edition, ISBN978-0-13-189080-0, 2008

[4] O.C. Zienkiewicz, R.L. Taylor, The Finite Element Method for Solid and Structural Mechanics, 6th Edition, ISBN 0-7506-6321-9, 2005